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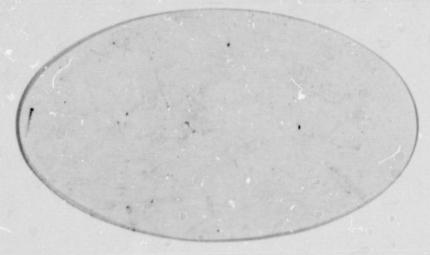
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N83-35002

PRESSURE MODIFICATION TO SPACE SHUTTLE
SYPRAULIC PUMP Final Technical Report (Abex
Cont., Oxnard, Calif.) 35 p HC A03/MF A01

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Abex Corporation - Aerospace Division 3151 W. 5th St., Oxnard, California 93030





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FINAL TECHNICAL REPORT
TO
NASA, L. B. JOHNSON SPACE CENTER
ON
SERVO CONTROLLED, VARIABLE PRESSURE
MODIFICATION TO
SPACE SHUTTLE HYDRAULIC PUMP
NASA CONTRACT
NAS 9-16622

AER-873 25 July 1983

Prepared by:

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H. H. Kouns Staff Engineer Approved by:

T. E. Sarphie Director of Engineering

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## <u>APPENDIX</u>

#### INTRODUCTION

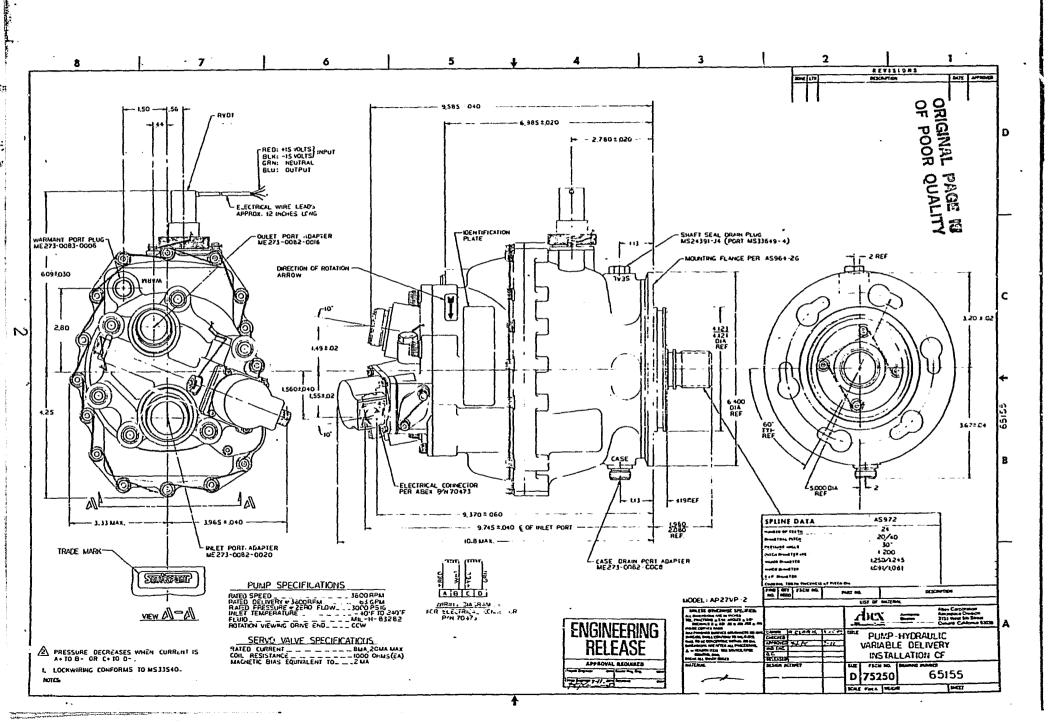
This report describes the modifications made to a standard model AP27V-7 (Abex P/N 65111) Space Shuttle hydraulic pump under contract NAS 9-16622 for the L. B. Johnson Space Center at Houston, Texas.

#### **OBJECTIVE**

The objective of the contract is to modify the constant pressure control of the model AP27V-7 hydraulic pump to an electrically controlled variable pressure setting compensator. In addition, the conversion is to include a hanger position indicator for continuously monitoring hanger angle. Also to be furnished is a simplex servo driver for controlling the pressure setting servovalve, as well as a support data package. Pump is then to be used to evaluate integrated performance on an "iron bird" flight control system application.

## DESCRIPTION OF PUMP MODIFICATIONS

Drawing number 65155 shows the pertinent overall and installation dimensions of the model AP27VP-2 pump. All basic port dimensions are unchanged from the -7 model. overall length has been increased to 10.8 inches and the vertical height from the pump center line has been increased to 6.09 inches to accommodate the RVDT unit. Other specifications remain unchanged.

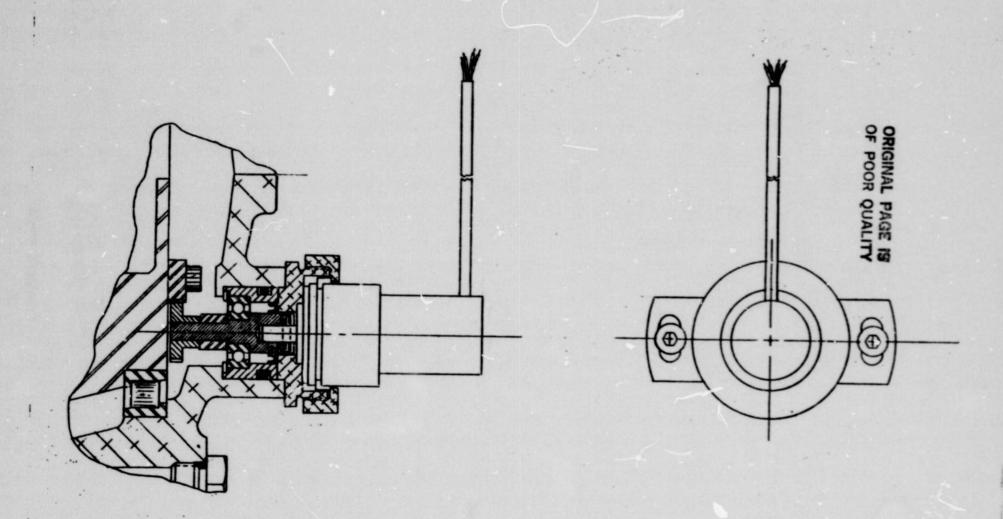


The basic unit furnished by NASA was a modified version of the standard Shuttle hydraulic pump (part number 65111, S/N 152294). The pump was disassembled and inspected for wear; all parts were found to be in excellent condition. The port plate was discarded, however, because it was a non-standard configuration (a result of an earlier special modification). A new port plate of standard configuration was substituted.

The pump mounting flange and hanger were then modified for adapting the RVDT (rotary variable displacement transducer) unit which is mounted on a special pad at the end of the mounting flange. Figure 1 is a partial cross section of the RVDT and mounting pad. The hanger angle position shaft is driven by a pinion gear which engages a segment gear at the end of the hanger. The resulting drive train ratio is 1:3. The other end of the position shaft is connected through a flexible coupling to the RVDT. The shaft is supported by a ball bearing and is sealed externally with a lip seal.

The pump front housing was modified by the addition of trunnion bearing stops which were welded and machined to form cradles above each bearing. These stops limit hanger lift under start up or adverse, no-load conditions to a maximum of .010 inches. This prevents disengagement of the hanger position indicator gears.

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ROTARY VARIABLE DISPLACEMENT TRANSDUCER

Figure 1

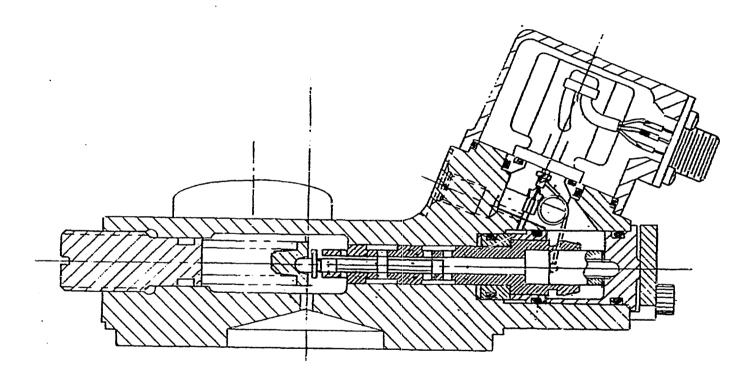
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A new port cap was designed and fabricated to give point to point inlet and outlet port locations and sizes per the AP27V-7 installation requirements and to accommodate the mounting of the servovalve. The design included the proven variable pressure control concept adapted from a similar size Abex pump.

Figure 2 is a schematic cross section of the pressure control mechanism and servovalve. The normally stationary sleeve of the compensator is now movable. The position of the sleeve, as shown, is in the maximum set pressure position. In this mode the compensator spool is load-adjustable with the normal adjusting screw-spring loading mechanism; maximum operating pressure is adjusted with the sleeve in this position. Fitted to the sleeve at the larger end is a floating piston grounded against the end cap. The net area of this piston is biased against the step area on the outside of the control sleeve. Pressure on the sleeve step area is controlled by the servoyalve through the receiver. If the servoyalve receives a command to reposition the sleeve to the right (lower pressure), the jet repositions to increase the receiver pressure and the sleeve moves to the right until rebalance is achieved between the floating piston of the sleeve and the step area of the sleeve. A position feedback spring between the sleeve and the servoyalve jet pipe closes the command loop of the control system. Repositioning the

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SERVO-CONTROLLED VARIABLE PRESSURE COMPENSATOR

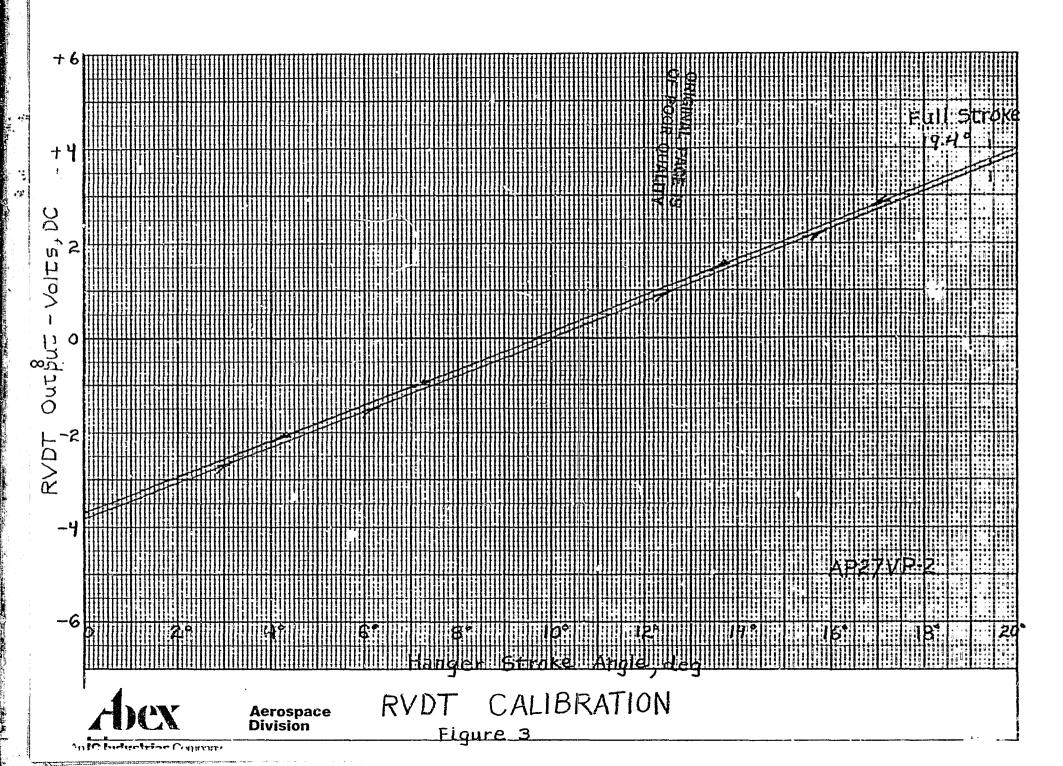
Figure 2

compensator sleeve to the right is equivalent to decreasing the spool spring load by unscrewing the adjustment screw an equivalent amount to the left. Basically, the compensator spool pressure, the floating piston pressure, and servovalve supply pressure are all equal to pump discharge pressure. The receiver pressure and the step area pressure are servovalve controlled.

The control concept is "fail safe" in that any interruption of electrical signal (zero amperage) or hydraulic supply pressure (plugged filter) to the servovalve results in a pressure bias on the compensator sleeve such that it immediately repositions against the stop to the left (high pressure setting).

#### RVDT CALIBRATION

Figure 3 is a calibration curve of the RVDT output voltage vs hanger angle of the pump. The voltage change is linear from the zero-stroke hanger angle to the maximum-stroke angle of 19.4 degrees. RVDT voltage outputs are -3.8 volts and +3.66 volts, respectively. At elevated pump temperatures, the maximum stroke angle of the hanger increases slightly  $(0.1 - 0.2^{0})$ , as will the voltage output of the RVDT.

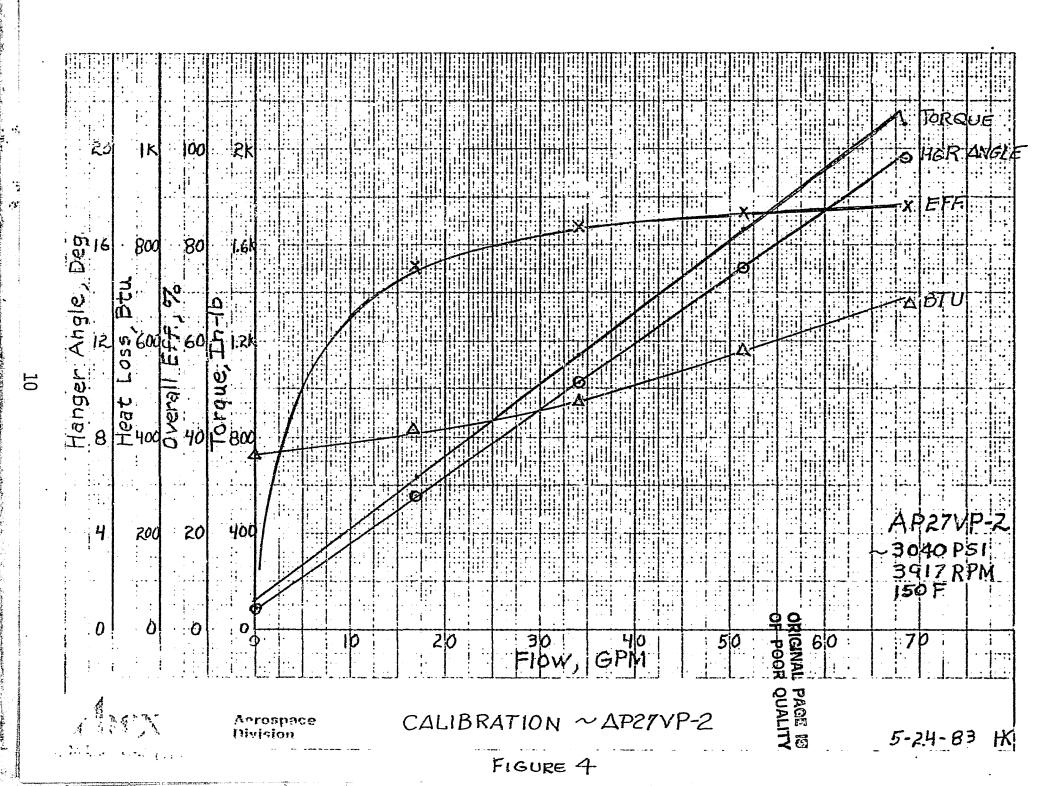


### PUMP PERFORMANCE & RESPONSE CHARACTERISTICS

A series of pump calibration data were taken on the AP27VP2 unit at 3917 rpm and at inlet temperatures of 150 F and 225 F. Torque and hanger position voltages were recorded at discharge pressure levels of 3000, 2000, and 1000 psi and at flows from full flow to zero gpm in 25 percent intervals. The results of these data and pertinent calculations are shown by the calibration curves, Figures 4 through 9.

Performance of the unit at the 3000 psi level is essentially unchanged. Overall efficiency at 60 gpm is 87.5 percent, and heat rejection at 5 and 15 gpm is 380 btu/minute and 400 btu/minute, respectively, with an inlet temperature of 150 %. At the high inlet of 225 F, the efficiency at 60 gpm is 88 percent, and the heat rejection is 330 btu/minute and 332 btu/minute, respectively. At 225 F inlet, and 1000 psi discharge pressure, the comparable heat rejection at 5 and 15 gpm is 200 btu/minute and 240 btu/minute, respectively. This represents a 40 and 32 percent energy savings, respectively, at the lower pressure. Similar energy savings result throughout the complete flow range. Figures 10 and 11 are typical calibration curves of standard AP27V-7 Shuttle pump, included for comparison purposes.

The dynamic response of the pump output control circuit was determined by oscillograph traces of the discharge pressure as the electrical signal to the servovalve was interrupted



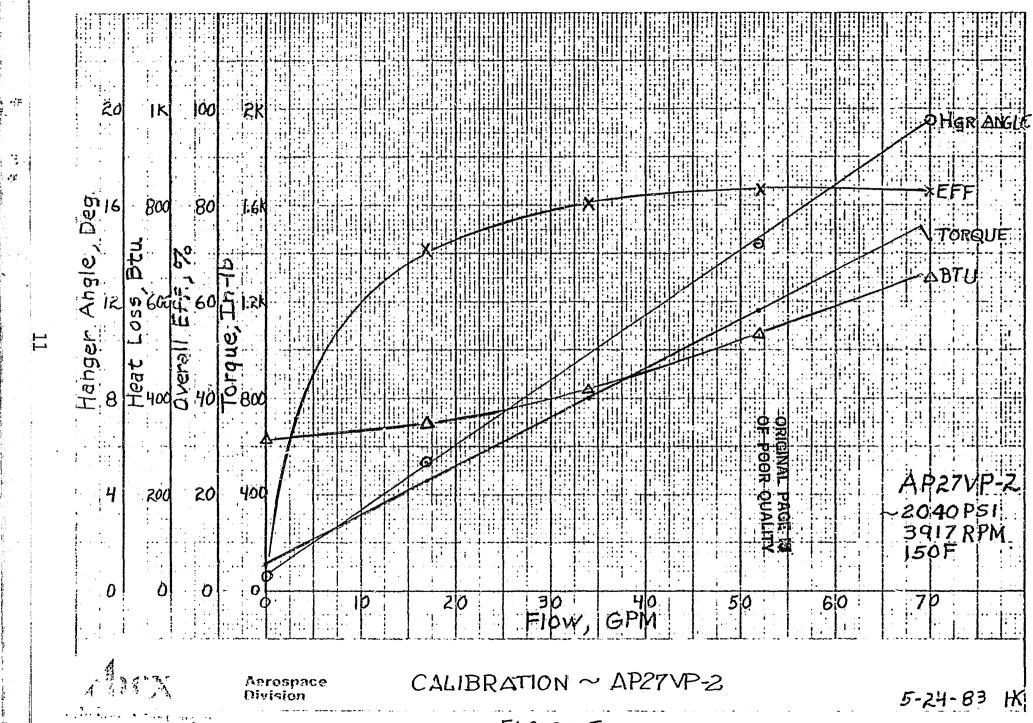


FIGURE 5

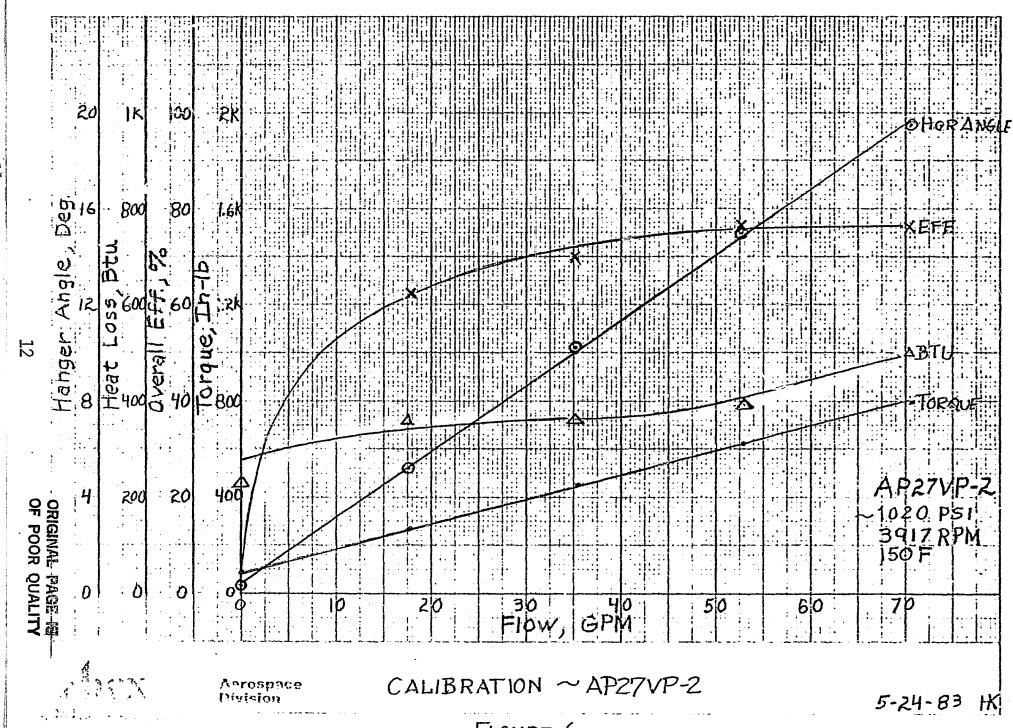


FIGURE 6

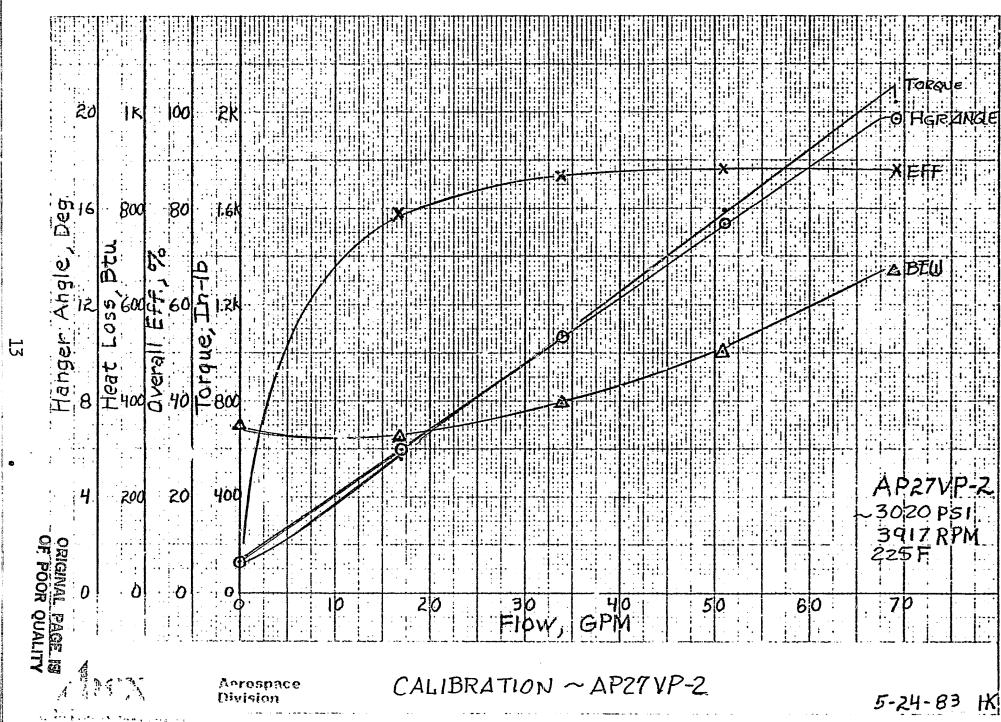


Figure 7

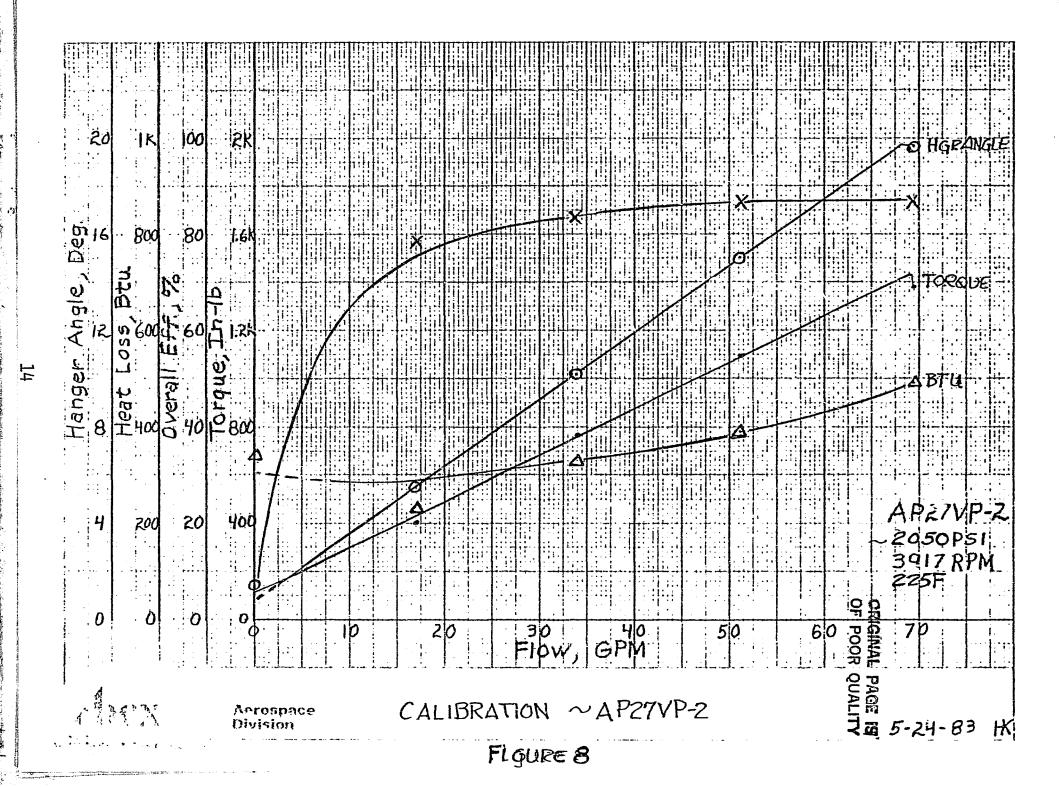
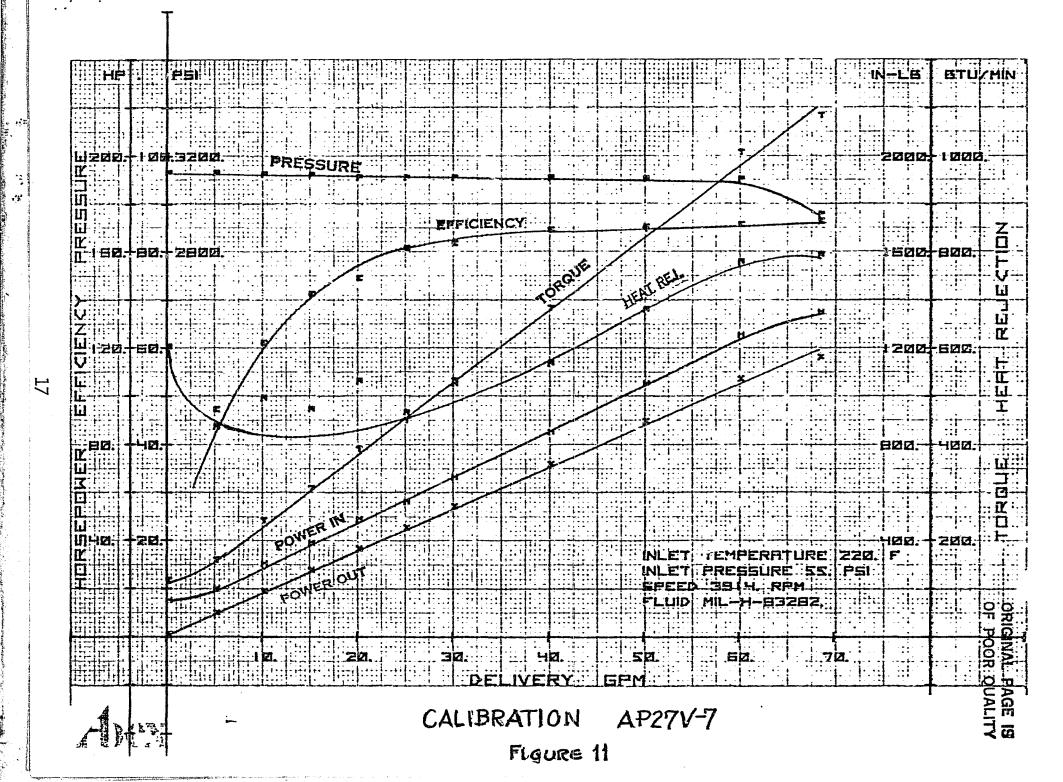


FIGURE 9

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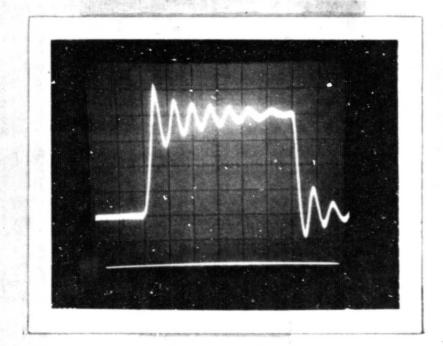
and then restored. Traces were obtained at pump flows of 5 and 15 gpm and speeds of 1800 and 4000 rpm in a system volume of approximately 150 in<sup>3</sup>. Pressure recovery time (1000 psi to 3000 psi) varied from 47 ms (milliseconds) at the higher speed and lower flow to 107 ms at lower speed and the higher flow rate. Pressure stability was achieved well within the one second requirements of the military specification. Pressure decay times in most cases was approximately 70 ms (no requirement). Figures 12 and 13 are typical response traces photographs.

Pressure control hysteresis was determined at pump speeds of 1800 and 4000 rpm, with discharge flows of 5 and 15 gpm, and at an inlet temperature of 225 F. Control current hysteresis was generally less than 0.1 milliampere. Figures 14 through 17 are typical performance plots of the electronic pressure control hysteresis.

## CONCLUSIONS

Test results and data analysis confirm that the modified AP27VP-2 hydraulic pump meets or exceeds all of the requirements and objectives as described in the NASA contract.

Normal (3000 psi) pump performance parameteres are unchanged --output flow, overall efficiency, heat rejection, response, etc., are unaffected by the modifications. The expected



5 gpm , 1000 -3000 -1000 psi

15 gpm, 1000-3000-1000psi

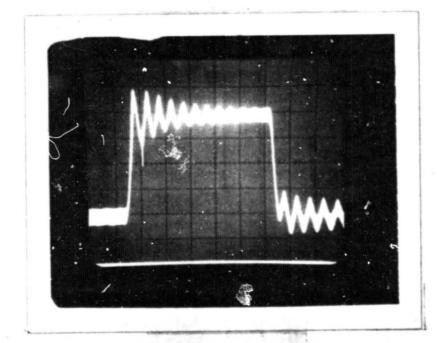
Speed ~1800 rpm Sweep time ~200ms/block Pressure ~ 500 psi/block

RESPONSE TIME - AP27VP-2

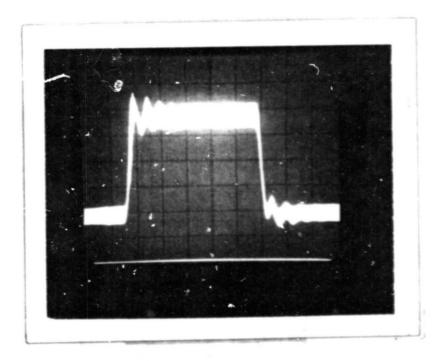
Figure 12

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5 gpm , 1000 -3000 -1000 psi

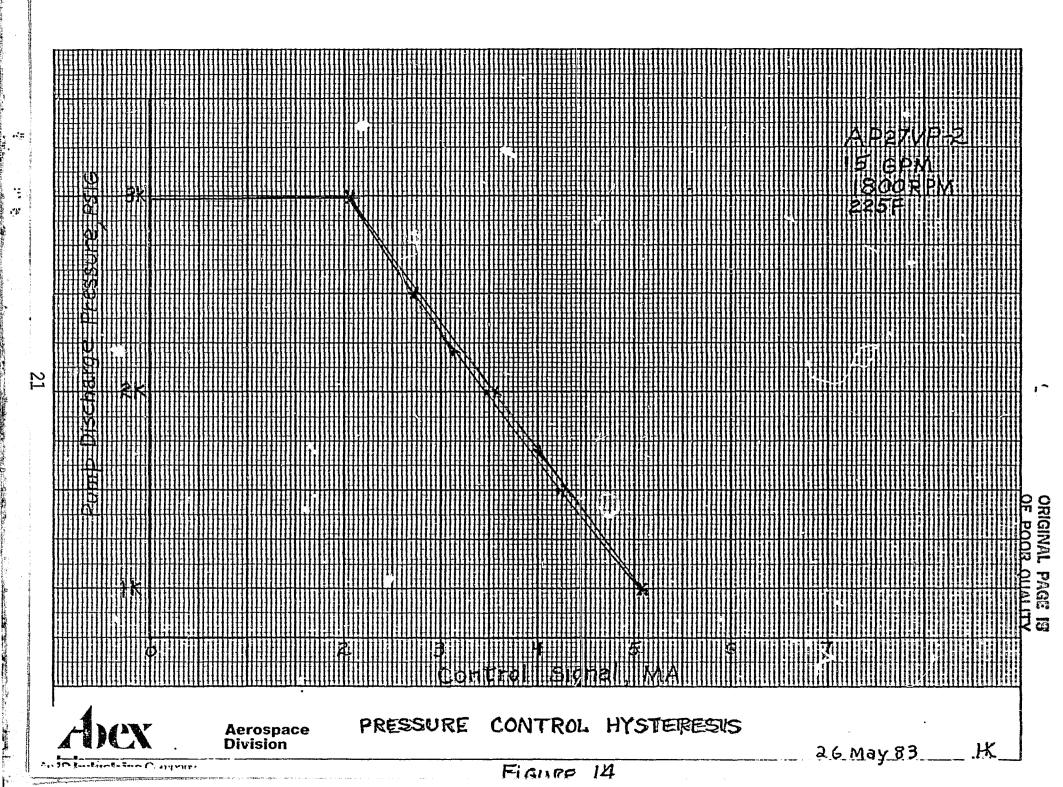


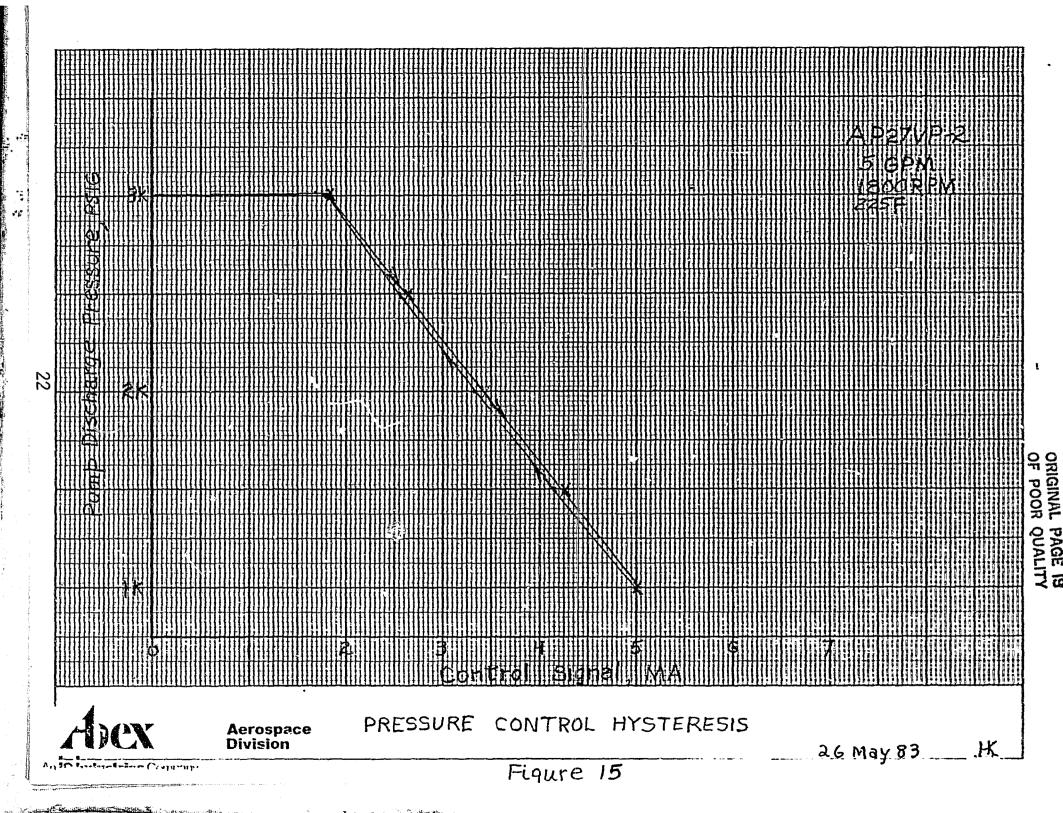
15 gpm, 1000-3000-1000psi

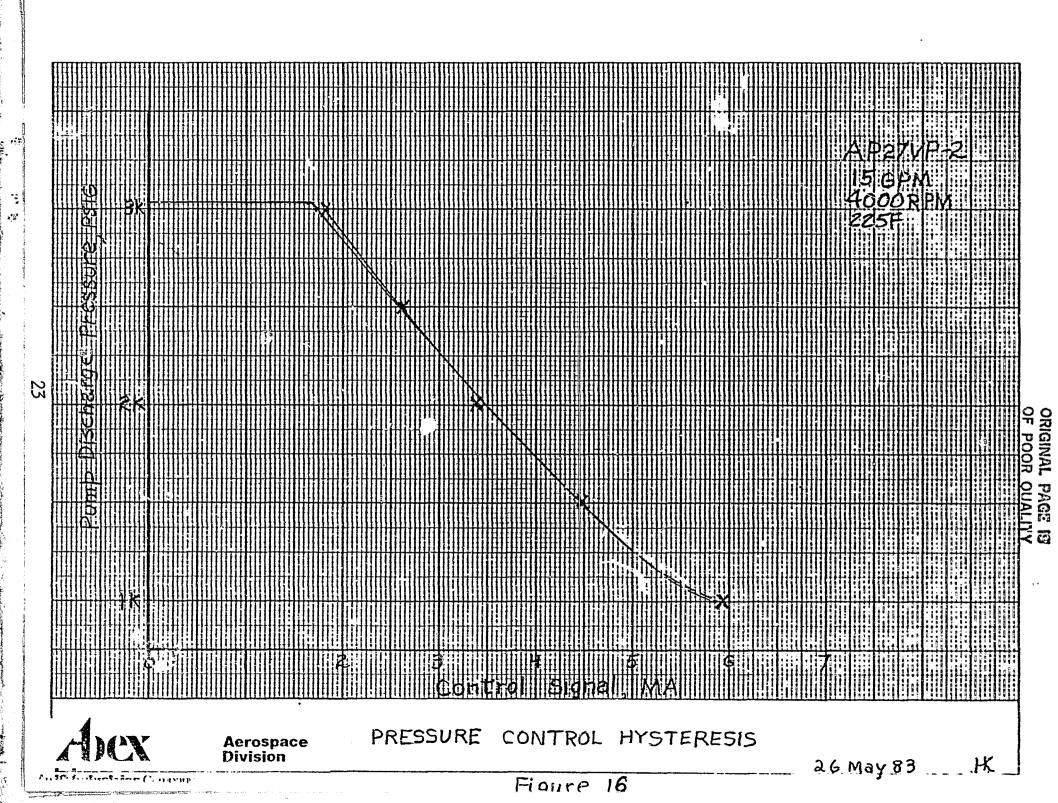
Speed ~4000 rpm Sweep time ~200ms/block Pressure ~ 500 psi/block

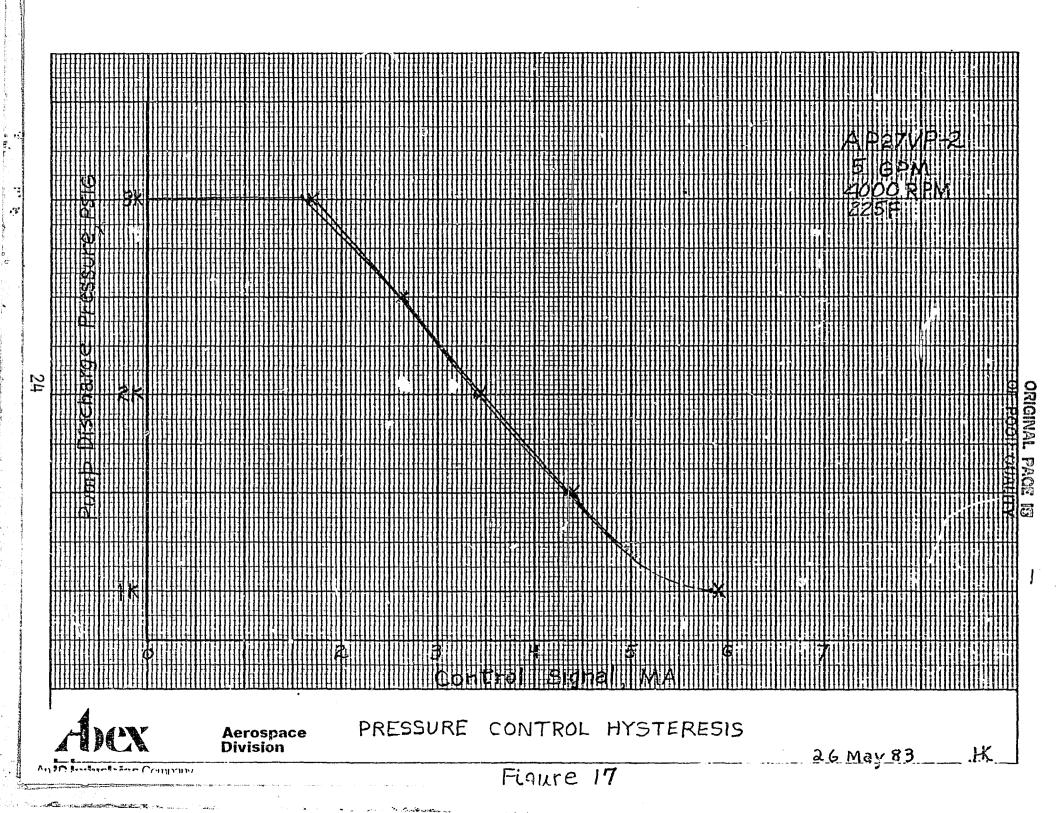
RESPONSE TIME - AP27VP-2

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savings in heat rejection (energy reduction) are confirmed at the lower pressure levels. The electronic pressure level control functions properly with little hysteresis and the RVDT accurately tracks hanger angles under all conditions.



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